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Research on optical 32QAM-OFDM-PON access scheme with different numbers of sub-carriers using DMT modulation



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Abstract

An optical 32QAM-OFDM-PON system with different numbers of sub-carriers using discrete multitone (DMT) modulation and demodulation is designed and demonstrated by experiment. Electron-optic generation, directly photoelectric detection, and electrical self-mixing reception of 32QAM-OFDM downstream signals are achieved. 5Gb/s 32QAM-OFDM downlink signals with different numbers of sub-carriers are successfully transmitted over 42 km SMF-28. Peak-to average power ratio (PAPR) characteristic, computational complexity and bit error rate (BER) performance are analyzed. The results show that the sub-carriers numbers of 32QAM-OFDM downlink signals should be carefully selected according to the actual requirements, if spectral efficiency, PAPR characteristic, computational complexity and receiver sensitivity are considered.

Keywords: PON, 32QAM-OFDM, DMT, PAPR, BER

Introduction

In recent years, orthogonal frequency-division multiplexing (OFDM) has been widely adopted in many optical access areas, such as OFDM modulated WDM-PONs [1–3] and OFDM-RoF systems [4-9], due to its high spectral efficiency, tolerance to dispersion and flexibility to dynamically bandwidth [1, 10, 11]. At present, few researchers focus on the reception of different m-quadrature amplitude modulation (QAM) (m = 4, 16, 32, and 64) OFDM downstream signals using self-mixing reception in optical access networks. For simplifying the optical access system configuration and reducing cost budget, we have designed and experimentally demonstrated two kinds of full-duplex 60GHz radio over fiber systems with 16QAM-OFDM downlink signals generated by discrete multitone (DMT) modulation and demodulation and received by self-mixing reception [10, 11]. But, few articles report on 32OAM or higher order QAM mapped OFDM optical signals with different numbers of sub-carriers applications in PON systems using DMT modulation and electrical self-mixing reception technique. In addition, although high spectral efficiency transmission and high sensitivity reception of access signals are the focus of attention, the computational complexity in the process of using digital signal processing (DSP) should also be considered. In this paper, we experimentally propose and demonstrate a novel self-mixing detection PON scheme using 5Gb/s 32QAM-OFDM downstream signals through DMT modulation and demodulation. Moreover, peak-to average power ratio (PAPR) characteristic, computational complexity and bit error rate (BER) performance are also analyzed, while different numbers of sub-carriers of 32QAM-OFDM downlink signals are selected.

Modulation and demodulation methods

As we know, one common method is that while passband OFDM system is used, the digital bit stream is converted first into an equivalent baseband signal, and then to a RF signal through subcarrier modulation. If

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DMT is utilized, the bandwidth of the generated electrical spectrum will be enlarged to twice range of the original signal, which is equal to the minimum value of the enlarged bandwidth using subcarrier modulation, where the output of the IFFT modulation is real instead of complex-valued [11]. The schematic diagrams of DMT modulation and demodulation of 32QAM-OFDM downlink signals in the electric field are shown in Fig. 1 as insets (a) and (b), respectively. The DMT is one special subclass of OFDM, using it the output signal after the inverse fast Fourier transform (IFFT) is real valued OFDM signal. The reason why DMT modulation is adopted is that, in traditional OFDM communication system, the time domain data vector is in the form of bipolar complex number, but optical fiber access systems with intensity modulation can only transmit positive real value signals. The DMT modulation and demodulation of 32QAM-OFDM signals is similar to the process in Ref. [12]. When this effective method is introduced in the optical access system, in-phase and quadrature (IQ) will be not required [1]. The system complexity and cost budget could be reduced, since high-frequency microwave source at the optical line terminal (OLT), local oscillator at the optical network unit (ONU) and analog RF components required for IQ modulation are omitted from the transceivers. Moreover, as the number of sub-carriers increases, if each sub-carrier signal is regarded as a remainder signal with random phase, the computational complexity of the DSP will be increased in the process of all sub-carriers superposing to form a DMT signal. And the envelope of the formed DMT signal will fluctuate, which will inevitably lead to a higher peak value, resulting in a higher PAPR value of the muticarrier signal. Therefore, the computational complexity and PAPR negative effects need to be discussed in the subsequent analysis.

Experimental setup and results

Figure 2 shows the experimental configuration. The linewidth of both two external cavity lasers (ECLs) is 100 kHz. The reason for using the ECL is that it can overcome the disadvantages of the traditional semiconductor laser, such as poor mode stability, large divergence angle and linewidth, and has the characteristics of high stability, small volume and high output power. Two 3paddle fiber polarization controllers (PCs) are connected to the back of the two ECLs through single mode optical fibers, and each PC is adjusted manually to ensure the highest output power of the two continuous light waves. The frequency tone spacing of the two generated free-running continuous wave lightwaves is 60GHz. The reason why 60GHz is selected is that it can be upgraded to be applied in millimeter wave ROF access systems in the future. A 32QAM-OFDM signal is generated offline and uploaded into one arbitrary wavelength generator (Tektronix AWG 710). In the experiment, DMT modulation and demodulation are used and the number of sub-carriers is dynamically optional (for example, 16, 32, 64, 128, 256, etc. are selected). The length of the cyclic prefix is 1/16 of the symbol time, and a training sequence is inserted every 100 symbols for channel estimation and time synchronization. One CW is modulated by one intensity modulator (LiNbO₃ Mach-Zehnder modulator, MZM) driven with the 5Gb/s 32OAM-OFDM signal amplified by one electrical amplifier (EA). The used MZM modulator ($V\pi = 3.6 \text{ V}$) is biased in the quadrature point and driven by by the 5Gb/s signal with a 1/2 half-wave voltage of 1.8 V for linear modulation. After electro-optic modulation, this 32QAM-OFDM signal is combined by one 3 dB optical coupler (OC) with the other CW without signal

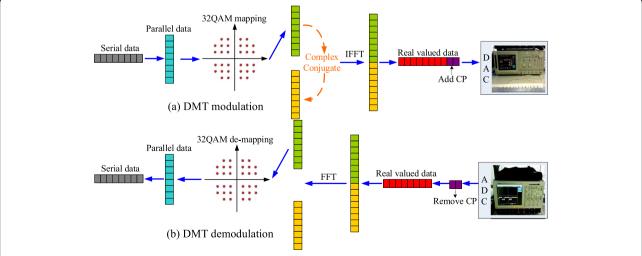


Fig. 1 Block diagrams of the DMT modulation (**a**) and demodulation (**b**) of 32QAM-OFDM signals. DMT: discrete multitone; IFFT: inverse fast fourier transform; FFT: fast fourier transform; DAC: Digital to analog converter; ADC: Analog to digital converter

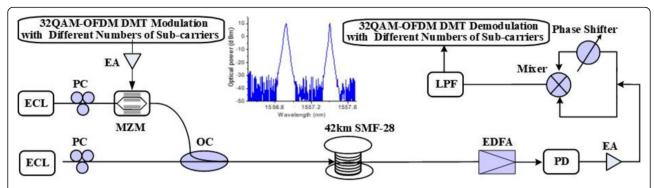
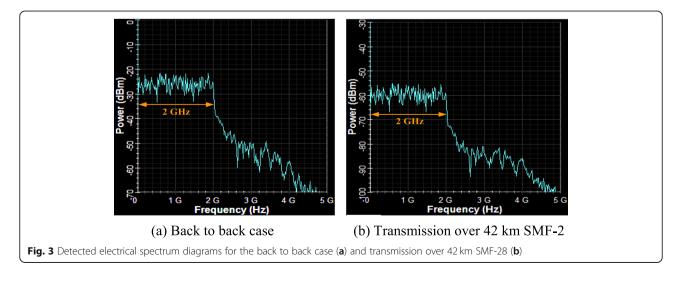


Fig. 2 Experimental setup. ECL: external Cavity Laser; PC: polarization controller; EA:electric amplifier; MZM: Mach-Zehnder modulator; OC: optical coupler; SMF: single mode fiber; EDFA: erbium-doped optical fiber amplifier; PD: photodetector; LPF: low pass filter

modulation. The measured optical spectrum diagram of the downlink signal before transmission is shown in the insert of Fig. 2. In the generated spectrum, one sideband is slightly broadened, which carries the modulated downstream optical signal. The downlink consists of 42 km single mode fiber (SMF-28) with an erbium-doped fiber amplifier after transmission (EDFA). Subsequently, one PIN PD with a 3 dB bandwidth of 70GHz and a DC responsivity of 0.6A/W is used to detect the signal after transmission. The two optical sidebands beat together in the PIN PD and generate a 60GHz mm-wave electrical signal. The converted electrical signal is amplified by one electrical amplifier with the bandwidth of 10GHz at the center frequency of 60GHz. After the electrical amplifier, the signal is directly mixed with itself. To match the RF phase information, one adjustable phase shifter was used for self-mixing detection. The generated baseband signal is filtered out by using a low pass filter (LPF). By a digital storage oscilloscope (Tektronix TDS6604), the downstream 32QAM-OFDM signal is obtained. The electrical spectrum diagrams for the back to back (BTB) case and transmission over 42 km SMF-28 are shown in Fig. 3 (a) and (b), respectively. It is clear to see, the electrical spectrum value of 5Gb/s 32QAM-OFDM signal is 2GHz, which is exactly equal to twice of the electrical spectrum value of the 32QAM-OFDM at the same bit rate using common baseband modulation. The electrical spectrum is extended using DMT method, and the result is the spectral efficiency is sacrificed. However, the DMT modulation and demodulation can eliminate the need for high-frequency microwave source at the OLT and local oscillator at the ONU, which will reduce cost budget, and achieve easy installation and maintenance. Moreover, the results also show the self-mixing detected 32QAM-OFDM signal is effective in this experiment.

One of the main drawbacks of the OFDM signal is its high PAPR [11, 13]. Using DMT modulation and demodulation with number of N (N = 16, 32, 64, 128, 256) sub-carriers, the measured complementary cumulative distribution function (CCDF) curves of the PAPR of 32QAM-OFDM are shown in Fig. 4. With increasing the number (N) of sub-carriers, there was a corresponding increasing in CCDF value under a certain PAPR threshold. It can be seen that 32QAM-OFDM signals with



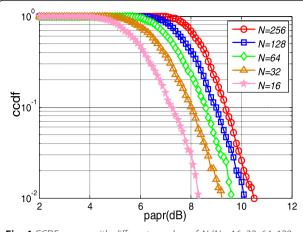


Fig. 4 CCDF curves with different number of N (N = 16, 32, 64, 128, 256) sub-carriers

small number of sub-carriers have lower PAPR probability than with great number of sub-carriers. Especially for N=16, the significant reduction in PAPR is observed. The generated 32QAM-OFDM signal with 16 subcarriers in reducing the PAPR is best using DMT modulation and self-mixing reception. But, in practice, the number of the sub-carriers can not be too few, because the OFDM signal with more sub-carriers has higher spectral efficiency. Another problem can not be ignored is the computational complexity in the DSP of the proposed scheme with different number of sub-carriers.

Figure 5 shows the amount of complex operations in the case of N = 16, 32, 64, 128, 256. It can be seen that the complex operations, including complex multiplications and additions are limited by the numbers of sub-carriers. To reduce the complex operations and PAPR simultaneously, we should choose as few as possible number of N sub-carriers. However, the number of the sub-carriers in the total transmission sequence can not be too few, since the generated

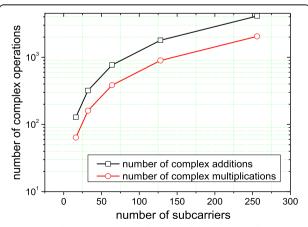


Fig. 5 Complex operations as a function of the number of *N* sub-carriers

signals with more sub-carriers has higher spectral efficiency, tolerance to dispersion and flexibility to dynamically bandwidth. Moreover, according to the research of existing literature, few researchers chose OFDM signal with lower number of sub-carriers for transmission. If we consider the influence of computational complexity, PAPR and spectral efficiency at the same time, an appropriate number of sub-carriers must be chosen.

Figure 6 shows the measured BER curves of 5Gb/s 32OAM-OFDM downlink signals (with 64, 128 and 256 sub-carriers). For the BTB case, regardless of the number of sub-carriers selected for application, the BER results are similar. After transmission over 42 km SMF-28, the receiver sensitivity (at a BER of 10⁻⁴) of the downstream signal with 64 sub-carriers is the best. Compared with the condition with 128 and 256 sub-carriers, the values of the power penalty at $BER = 10^{-4}$ will be reduced, which are almost 0.15 dB and 0.3 dB, respectively. The results of the above discussion seem to show that the downlink signal with 64 sub-carriers is more suitable for the actual applications, since the receiver sensitivity can be effectively enhanced than with 128 and 256 subcarriers. In combination with the previous discussion, we can see that the PAPR influence and the computational complexity is lower at this case. But, if we expect getting higher spectral efficiency, tolerance to dispersion and flexibility to dynamically bandwidth for 32QAM-OFDM signals application, we may choose using more sub-carriers. That is to say, we must make a trade-off selection according to the actual requirements of downlink access signals. Maybe the 32QAM-OFDM signal with 128 sub-carriers is a more suitable access signal, because its receiving sensitivity and spectral efficiency are relatively high, the PAPR value is not very large, and the computational complexity is not prominent.

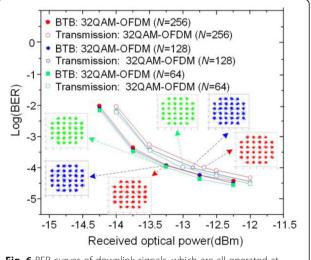


Fig. 6 BER curves of downlink signals, which are all operated at 5Gb/s (with 64, 128 and 256 sub-carriers)

Conclusion

In this paper, we have designed and experimentally demonstrated an optical 32OAM-OFDM-PON system with different numbers of sub-carriers. The introduced DMT modulation and demodulation, and the adopted selfmixing detection can effectively reduce system configuration and cost budget, since it eliminates the need for high-frequency microwave source at the OLT and local oscillator at the ONU. Moreover, using this scheme results in good dynamic sub-carriers bandwidth allocation, because different numbers of sub-carriers can be selected according to the actual application. PAPR characteristic, computation complexity, and BER performance of 32QAM-OFDM downlink signals with different numbers of sub-carriers are analyzed. This scheme is potentially valued in future PON networks applications, and can also be upgraded to support radio over fiber PON (RPON) applications while using one PIN PD with a 3 dB bandwidth of 70GHz cascaded by a pair of a pair of millimeter wave antennas.

Abbreviations

QAM: Quadrature amplitude modulation; OFDM: Orthogonal frequency division multiplexing; PON: Passive optical network; DMT: Discrete multitone; PAPR: Peak-to average power ratio; BER: Bit error rate; WDM-PON: Wavalength division multiplexing-passive optical network; DSP: Digital signal processing; IFFT: Inverse fast Fourier transform; IQ: In-phase and quadrature; ONU: Optical network unit; ECL: External cavity laser; ROF: Radio-over-fiber; MZM: Mach-Zehnder modulator; EA: Electrical amplifier; OC: Optical coupler; CW: Continuous-wave; SMF: Single mode fiber; EDFA: Erbium-doped optical fiber amplifier; PIN PD: Positive-intrinsic-negative photodiode; LPF: Low pass filter; BTB: Back to back; OLT: Optical line terminal; CCDF: Complementary cumulative distribution function

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Authors' contributions

Yufeng Shao conceived and designed the study. Yufeng Shao and Ying Long performed the system configuration, and wrote the manuscript. Yufeng Shao reviewed and edited the paper. All authors read and approved the manuscript.

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Availability of data and materials

All data and materials are fully available without restriction.

Competing interests

The authors declare that they have no competing financial interests.

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